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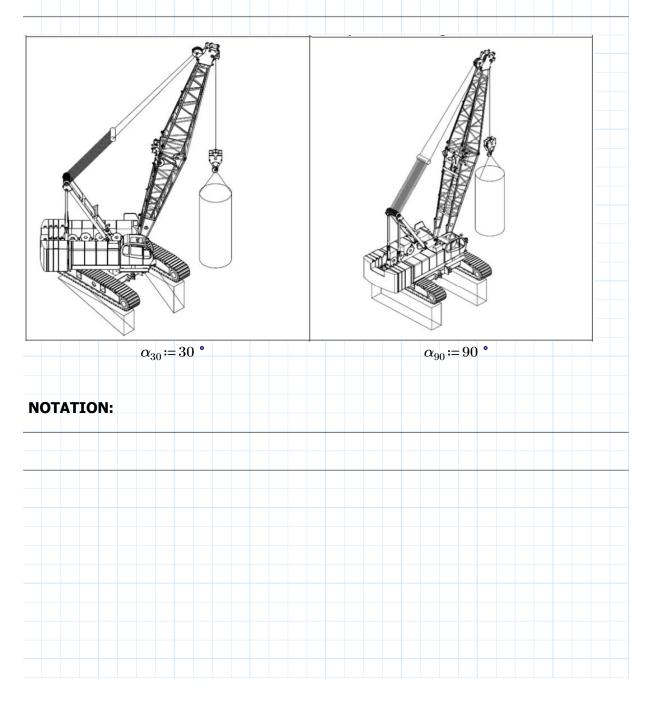
Crawler-Crane Track Pressures Calculation

Lift operation-1 as per case below:

Crawler crane operating over the side while picking up a load including hook block and slings 103.1 ton. The load is on the main hook at 7.3m radius. The crane using 39.6m boom length and has a 15.2-m jib mounted at 0° offset.

Check bearing pressure under the tracks on boom direction α_{90} (90 deg) and at α_{30} (30 deg).

Crane data:



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Solution Calculation-1: Find the boom angle. $R = t + L \cdot \cos(\alpha)$ $\alpha := a \cos\left(\frac{R-t}{L}\right) = 81.17 \ deg$ Calculation-2: The boom moment is given by: $M_b := W_b \cdot (t + L_b \cdot \cos(\alpha + \theta_b))$

 $M_b = 394.15 \ kN \cdot m$

Calculation-3:

The Jib moment + boom moment:

$$M_{bi} := M_b + W_i \cdot (t + L \cdot \cos(\alpha) + J_i \cdot \cos(\alpha + \mu_i))$$

 $M_{bi} = 444.750 \ kN \cdot m$

Calculation-4:

Calculate superstructure moment.

$$M_u \coloneqq M_{bj} + (W + W_r) \cdot R - W_u \cdot d_u$$

 $M_u = 5503.48 \ kN \cdot m$

Calculation-5:

The vertical load

$$V_u \coloneqq W_b + W_i + W + W_r + W_u$$

 $V_u = 2062.87 \ kN$

Calculation-6:

The moments over the front side ($\alpha = 90^{\circ}$) are:

$$M_{nf.90} = M_u \cdot \cos\left(\alpha_{90}\right)$$

 $M_{nf.90} \coloneqq 0 \ \mathbf{kN} \cdot \mathbf{m}$

 $M_{ns.90} \coloneqq M_u \cdot \sin(\alpha_{90})$

$$M_{ns.90} = 5503.48 \ kN \cdot m$$

 Calculation-7:

 Machine vertical load is:

 $V := V_u + W_c$
 $V = 2637.85 \ kN$

 Case-1: Find the track pressures when the horizontal operating angle $\alpha = 90^\circ$.

Calculation-8:

When Slew boom direction at 90 deg., $M_{nf} = 0$, therefore e = 0

therefore e = 0.

$$\begin{split} e_{\alpha.90} &\coloneqq \frac{M_{nf.90}}{V} & e_{\alpha.90} = 0 \ m \\ \\ l_{\alpha.90} &\coloneqq 3 \left(\frac{d_l}{2 - \frac{e_{\alpha.90}}{m}} \right) & l_{\alpha.90} = 10.965 \ m \\ \\ l_{\alpha.90} &> d_l \rightarrow 10.965 \cdot m > 7.31 \cdot m \end{split}$$

Conclusion:

 $l_{\alpha,90} > d_l$ therefore the pressure diagram is trapezoidal. Using Eq. (5.30)

Calculation-9:

Calculate reaction force at heavily side (R_h) and lightly side (R_l) $R_{h.90} \coloneqq \frac{V}{2} + \frac{M_{ns.90}}{d_t}$ $R_{h.90} \equiv 2375.26 \text{ kN}$ $R_{t.00} \coloneqq \frac{V}{2} - \frac{M_{ns.90}}{d_t}$

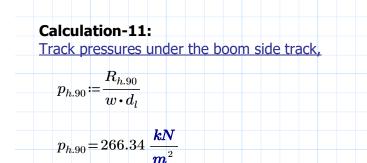
$$\frac{1}{2} \frac{1}{2} \frac{1}$$

 $R_{l.90} = 262.59 \text{ k/N}$

Calculation-10:

Track pressures. With e = 0, pressure will be uniform along each track ($p_{max} = p_{min} = p$). Track pressures under counterweight side track,

$$p_{l.90} \coloneqq \frac{R_{l.90}}{w \cdot d_l} \cdot \left(1 + \frac{6 \cdot e_{\alpha.90}}{d_l}\right)$$
$$p_{l.90} = 29.44 \frac{kN}{m^2}$$



NOTE: The pressures calculated are for the loaded lift case case above only, and over the side while picking load at ($\alpha = 90 \text{ deg}$).

Case-2: Find the track pressures when the horizontal operating angle $\alpha = 30^{\circ}$.

Solution

Calculation-12:

Rotation of the superstructure causes a redistribution of upper moments and of track loadings.

$$M_{nf,30} \coloneqq M_u \cdot \cos(\alpha_{30})$$

 $M_{nf.30} = 4766.15 \ kN \cdot m$

 $M_{ns.30} \coloneqq M_u \cdot \sin\left(\alpha_{30}\right)$

 $M_{ns.30} = 2751.74 \ kN \cdot m$

Calculation-13:

Calculate reaction force at heavily side (R_h) and lightly side (R_l) Using Eq. (5.30)

$$R_{h.30} \coloneqq \frac{V}{2} + \frac{M_{ns,30}}{d_t}$$

$$R_{h.30} \equiv 1847.09 \ kN$$

$$R_{l.30} \coloneqq \frac{V}{2} - \frac{M_{ns,30}}{d_t}$$

$$R_{l.30} \equiv 790.76 \ kN$$
Calculation-14:
Calculate the eccentricity:

$e_{\alpha.30} \coloneqq \frac{M_{nf.30}}{V}$	$e_{\alpha.30} = 1.8 \ m$
V V	

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